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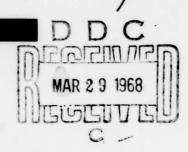
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A DIVISION OF GENERAL DYNAMICS CORPORATION

SAN DIEGO

REPORT ZP-7-022 TN

DATE 2-14-56

MODEL XM-65

TITLE

ANALYSIS OF MISSILE

TANK GEOMETRIES

ZP-7-022 TN

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	Model 7 - Preliminary Design and Systems
PREPARED BY P. D'Vincent	GROUP Analysis

\_\_\_\_\_REFERENCE\_\_\_

CHECKED BY \_\_\_\_\_ APPROVED BY Weff A. Bluid

NO. OF PAGES 36

REVISIONS

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ANALYSIS
PREPARED BY
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DATE 2-14-56

#### FOREWORD

This is a technical note pertaining to missile tank geometry.

It provides a list of formulas that may be referred to in reports

and other technical papers where their development is incidental.

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DATE 2-14-56

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#### SIDMARY

Mathematical relations are presented pertaining to various missile tank and bulkhead configurations. Although some of these relations are available in handbooks, they are included in this technical note together with a number of newly derived formulas. In this manner a comprehensive summary of equations is obtained, permitting rapid computation of volumes, surfaces and other geometric characteristics of a great variety of shapes.

The purpose of this technical note is to eliminate the need for repeating the derivations of frequently used equations in preliminary design and layout of missiles.

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#### INTRODUCTION

Reports concerning missile tank geometry have been compiled and it is expected that studies of this sort will continue. The studies indicate the necessity for a list of reference formulas applying to tank geometry that may be drawn from and referred to, eliminating the need of developing them within a report or the repetition of their development in related reports. Although it is felt proper to make calculations within a report, geometric formula development is incidental at the time of writing and should be available elsewhere.

This technical note is presented for the purpose of fulfilling this requirement and effort has been made to include a broad range of mathematical expressions to meet the needs of missile tank designers.

These formulas presented consist of mathematical expressions for tank and bulkhead volumes, their surface areas and other pertinent geometric information that is not readily available in standard handbooks. Formulas for partially filled tank shapes are included along with those of partially filled bulkheads.

In general, this report is compiled for use with studies pertaining to the SM-65 vehicle, however, it includes geometries for other shape tanks and bulkheads that may be used in future development studies.

No attempt is made by this report to qualify the choice of any particular tank or bulkhead.

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#### INTRODUCTION (cont d.)

The first part following this introduction contains a comprehensive list of formulas together with reference numbers which may be referred to in technical studies. Each of these formulas refer to its origination whether "classic" or whether derived within this report. If it is derived within this report, its location is referred to by page number.

The second part is devoted to the derivation of the uncommon formulas referred to in the first section. They are presented in a form that gives the designer an understanding or the fundamental derivation and allows him to change the formula's original parameters without time consuming effort.

The formulas contained in this report have been checked.

However, errors may exist and their appearance should be brought to
the authors attention for correction.

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# PART

SUMMARY EQUATIONS

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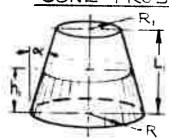
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VT IS TOTAL VOLUME ST IS TOTAL SURFACE ALEA

## CONE FRUSTUM TANK REF. PAGES 647

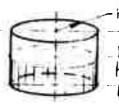


(1) 
$$V_T = \frac{\pi}{3 \text{TAN} \propto} \left( R^3 - R_1^5 \right)$$

(2) 
$$S_{\tau} = \frac{\pi L_{1}(R, +R)}{\cos x} *$$
  
=  $\pi (R+R_{1}) \sqrt{L_{1}^{2} + (R-R_{1})^{2}}$ 

(3)  $V(ofh_i)=11h_i(R^2-Rh_iTAN \propto +\frac{1}{3}h_i^2TAN^2 \propto)$ 

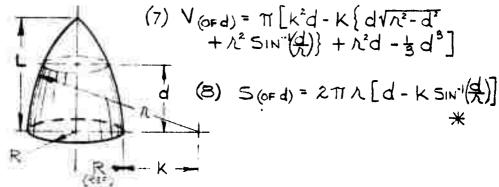
## CYLINDRICAL TANK (CLASSIC FORMULAS)



$$h = (4) V_T = \pi R^2 L$$
  
 $h = (5) V_{(0=h)} = \pi R^2 h$ 

(6) 5, = 2 TRL \*

## OGIVE TANK (CIRCULAR) REF. PAGE 8



\*NOTE . - TANK ENDS ARE NOT INCLUDED IN SURF. AREAS

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SPHERICAL BULKHEAD REF. PAGES 9,10 111

(11) 
$$\Lambda = \frac{H}{2} + \frac{R^2}{2H}$$
  
(12)  $S_7 = 2\pi \Lambda H *$ 

Use equ ? TWICE (13) 
$$V(oFt) = TId [(\Lambda^2 + h^2) - d(3d+h)]$$
  
(13) in ETROR.  
 $h = \Lambda - H$  OR  $h = \sqrt{\Lambda^2 - R^2}$ 

ELLIPTICAL BULKHEAD REF. PAGES 12,13+14

(IN CYLINDRICAL TANK)

(I4) 
$$V_7 = \frac{2}{3} \pi R^2 \alpha$$

(I5)  $V_{(OF h)} = \pi h \left(\frac{R}{\alpha}\right)^2 \left(\alpha^2 - \frac{1}{3}h^2\right)$ 

(16) 
$$V_{(OF h)} = \pi h \left(\frac{R}{a}\right)^2 \left(a^2 - \frac{1}{3}h^2\right)$$

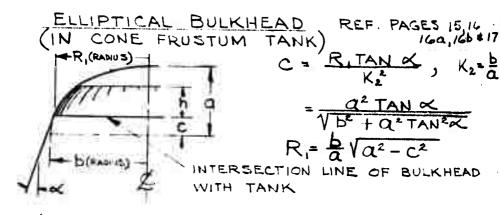
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(16)  $S_7 = \pi \left\{a\sqrt{c_1a^2 + R^2} + \frac{R^2}{|C_1|} \left[Log(a\sqrt{c_1 + 1c_1a^2 + R^2}) - LogR\right]\right\}$ 

(17) RADIUS OF CURVATURE (P) DIST. X ABOVE BASE PLANE  $\beta = \frac{\left[R^2 + K_1^2 X^2 (K_1^2 - 1)\right]^{\frac{1}{2}}}{\|Y\|^2 \|D\|^2}$ 

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X : ANGLE OF CONE FRUSTUM TANK

(18) V<sub>T</sub> (TOTAL VOL. OF BULK'D FROM BASE [TANK'S INTERSECTION] TO APEX)
$$= \pi \left(\frac{b}{a}\right)^2 \left[a^2(a-c) + \frac{1}{3}(c^3-a^3)\right]$$

(19) V (VOLUME FROM BASE TO h")
$$= \pi \left( \frac{b}{a} \right)^{2} \left[ a^{2} (h-c) + \frac{1}{3} (c^{5} - h^{3}) \right]$$

(20) S (SURFACE AREA OF BULK'D FROM BASE ETANK'S INTERSECTION] TO APEX)
$$S = \pi \left[ \alpha \sqrt{C_1 \alpha^2 + b^2} + \frac{b^2}{1C_2} \log(\alpha \sqrt{C_2} + \sqrt{C_2 \alpha^2 + b^2}) \right]$$

$$- C\sqrt{C_1C^2 + b^2} - \frac{b^2}{\sqrt{C_2}} Log(C\sqrt{C_2} + \sqrt{C_2C^2 + b^2})$$

OL : BULK'D MINOR SEMI AXIS (HEIGHT)

INTERSECTION WITH TANK = R, TAN 0 /K2 C, = K2 - K2 WHERE K2 = ba LOG IS BASE "A"

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$$V_{1} = \Pi \left\{ h(\Lambda^{2} + K^{2}) + K \left[ n \sqrt{\Lambda^{2} - L^{2}} + \Lambda^{2} \sin^{-1} \left( \frac{h}{\Lambda} \right) \right] - \frac{h^{3}}{3} \right\}$$

(CONE)

(21) 
$$V_{T} = V_{1} + V_{II}$$
  
 $V_{1} = \pi \{h(\Lambda^{2} + K^{2}) + K^{2}\} + K^{2}$   
 $V_{II} = \frac{1}{3} \pi \Lambda_{1}^{3} \text{Cot } \Theta$   
(22)  $S = S_{I} + S_{II}$ 

Co

$$S_{I} = 2\pi \Lambda \left[ K Sin^{-1} \left( \frac{h}{\Lambda} \right) + h \right]$$
 (forus)  
 $S_{II} = \frac{\pi \Lambda^{2}}{Sin\Theta}$  (cone)

PARABOLIC BULKHEAD REF. PAGES 20 # 21

a (23) 
$$V_T = \frac{1}{2} \pi R^2 a$$

(24)  $V_{(ofh)} = \frac{1}{2} \pi R^2 h [2 - \frac{h}{a}]$ 

R (25)  $S_T = \frac{1}{6} \pi Ra [(4 + \frac{R^2}{a})^{\frac{1}{2}} - (\frac{R}{a})^{\frac{1}{2}}]$ 

$$\beta = \frac{1}{2R\alpha} \left( 4\alpha X + R^2 \right)^{\frac{3}{2}}$$

$$X = \text{VERTICAL DIST FROM VERTEX TO}$$

$$\text{WHERE } P \text{ IS DESIRED (ON THE SURFACE)}$$

(27) RADIDS OF CURVATURE (P)

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Page 5

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BAN DIEGO, CALIFORNIA Medel\_\_\_\_\_

TORUS TANK

TORUS TANK REF PAGES 22 THRU 26

(28) 
$$V_T = 2\pi^2 b a^2 = 19.739 b a^2$$

$$V_{L} = 2\pi \alpha^{2} b \left\{ K \sqrt{1 - K^{2}} + \sin^{-1} K + \frac{\pi}{2} \right\}$$

$$K = \frac{h_{1}}{\alpha}$$

(32) INNER SKIN (2 hs WIDE)  

$$Si = 4 \pi \alpha \left[ b \sin^{-1} \left( \frac{hs}{a} \right) - h_s \right]$$

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PART II

DERIVATIONS

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## CONE FRUSTUM TANK

$$y = x \text{ TAN } \propto$$

$$VOLUME (ENCLOSE TANK), l_{2} = \frac{R}{TANX}$$

VOLUME (ENCLOSED FROM R, TO R)

$$V_{T} = \pi \int_{\ell_{1}}^{\ell_{2}} y^{2} dx = \pi \int_{\frac{R}{14NK}}^{\frac{R}{14NK}} x^{2} TAN^{2} x dx$$

$$= \pi TAN^{2} x \frac{X^{3}}{3} \int_{\frac{R}{14NK}}^{\frac{R}{14NK}} x^{2} TAN^{2} x dx$$

= 
$$\frac{11}{3 \text{ TAN } \propto (R^3 - R_1^3)} \circ R = \frac{11}{3} (R^2 + RR_1 + R_1^2)$$

SURFACE AREA

$$5 = \left(\frac{R_1 + R}{2}\right) \cdot 2\pi \cdot \frac{L_1}{\cos \kappa}$$

$$= \frac{\pi L_1(R_1+R_2)}{\cos \alpha} \quad \text{or} = \pi (R+R_1) L_1^2 + (R-R_1)^2$$

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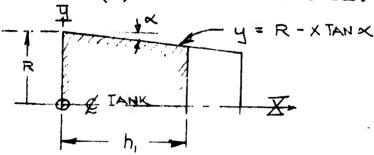
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## CONE FRUSTUM TANK (CONT'D)

PARTIALLY FILLED TANK IN TERMS OF BASE RADIUS (R), CONE ANGLE (K) AND HEIGHT OF LIQUID (A) ABOVE TANK'S BASE.



$$V = \pi \int_{0}^{h} y^{2} dx$$

$$= \pi \int_{0}^{h} (R - x \tan x)^{2} dx$$

= 
$$\pi \left[ R^2 X - R X^2 TAN \times + \frac{1}{3} X^3 TAN^2 \times \right]_0^{h_1}$$

= 
$$\frac{\text{Th}_{1}\left[R^{2}-Rh, TAN \times +\frac{1}{3}h^{2} TAN^{2} \times\right]}{\left[R^{2}-Rh, TAN \times +\frac{1}{3}h^{2} TAN^{2} \times\right]}$$

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OGIVE TANK (CIRCULAR)
(RADIUS NOSE)

$$x^{2} + (y + h)^{2} = h^{2}$$

$$y = -h + \sqrt{h^{2} - x^{2}}$$

$$dy = -x (h^{2} - x^{2})^{-\frac{1}{2}}$$

VOLUME: (ENCLOSED TO "d")  

$$V = \pi \int_{0}^{d} (-\lambda + \sqrt{\lambda^{2} - x^{2}})^{2} dx$$

$$= \pi \int_{0}^{d} (-\lambda^{2} - 2\lambda + \sqrt{\lambda^{2} - x^{2}} + \lambda^{2} - x^{2}) dx$$

= 
$$\pi \left[ h^2 x - 2h \cdot \frac{1}{2} \left( x \sqrt{\Lambda^2 - x^2} + \Lambda^2 \sin^2(\frac{x}{\Lambda}) \right) + \Lambda^2 x - \frac{1}{3} x^3 \right]_0^d$$
  
=  $\pi \left[ h^2 d - h \left( d \sqrt{\Lambda^2 - d^2} + \Lambda^2 \sin^2(\frac{x}{\Lambda}) \right) + \Lambda^2 d - \frac{1}{3} d^3 \right]$ 

SURFACE AREA (TO d) +  $\chi^2 d - \frac{1}{3} d^3$   $5 = 2\pi \int_0^d (-h + 1/(\lambda^2 - x^2)) \left[ 1 + \frac{x^2}{(\lambda^2 - x^2)^2} \right] dx$  $= 2\pi \int_0^d (-h + 1/(\lambda^2 - x^2)) \left[ \frac{h}{\sqrt{\lambda^2 + x^2}} \right] dx$ 

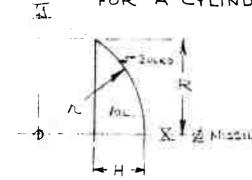
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SPHERICAL BULKHEAD

(THE FOLLOWING APPLIES TO A BULK'D FOR A CYLINDRICAL OR TAPERED TANK)



$$X^{2} + y^{2} = \lambda^{2} - X^{2}$$

$$(\lambda^{2} + y)^{2} + R^{2} = \lambda^{2} \quad \text{or} \quad \lambda^{2} \cdot 2\lambda H + H^{2} + R^{2} = \lambda^{2}$$

$$\lambda = \frac{H}{2} + \frac{R^{2}}{2H}$$

10

VOLUME

IN TERMS OF BULK'D HEIGHT (H) & RADIUS (A)

$$V = \pi \int_{A-H}^{A} y^2 dx - \pi \left( \frac{\chi^2 - \chi^2}{2} \right) dx$$

$$= \pi \left( \frac{\chi^2 \chi - \frac{\chi^2}{2}}{2} \right) \Big|_{A-H}^{A}$$

IN TERMS OF BULK'D HEIGHT (H) & TANK RAD (R)

A = # + R IN THE ABOVE FORMULA V = 6 7 H [H2 + 3R2]

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### SPHERICAL BULKHEAD (CONT'D)

### SURFACE AREA

$$x^{2} + y^{2} = \Lambda^{2}$$

$$2 \times dx + 2y dy = 0$$

$$dy = -\frac{x}{y}$$

$$5 \cdot 2\pi \int_{\lambda_{2}h}^{\lambda_{2}} y \sqrt{1 + \left(-\frac{x}{3}\right)^{2}} dx$$

FOR HEMISPHERE H . A

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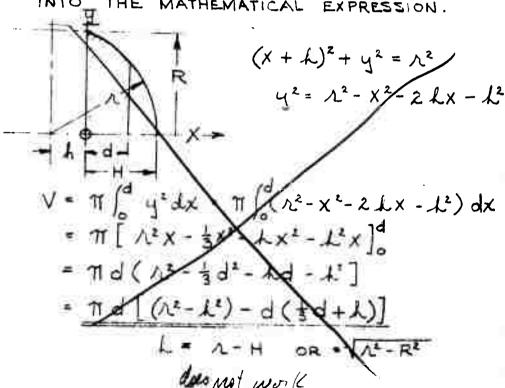


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### SPHERICAL BULKHEAD (CONT'D)

NOLUME OF LIQUID IN PARTIALLY FILLED BULKD
IN TERMS OF LIQUID DEPTH (d), BULK'D
RADIUS (L) AND DIST. (L) WHICH IS THE
DISTANCE BETWEEN THE BULK'D BASE
AND THE CENTER POINT OF THE BULK'D
RADIUS.

NOTE: IT IS DESIRABLE TO SHIFT THE X
AXIS TO THE BULK'DS BASE FOR REASONS OF
SIMPLIFICATION WHEN (L) IS INTRODUCED
INTO\_ THE MATHEMATICAL EXPRESSION.



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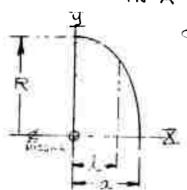
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### ELLIPTICAL BULKHEAD

VOLUME (ENCLOSED BY THE BULKHEAD IN A CYLINDRICAL TANK)



GEN. ELLIP. EQUATION
$$\frac{X^2}{K^2} + \frac{y^2}{K^2} = 1$$

$$y^2 = R^2 - (K_1 X)^2$$
  
 $K_1 = R/a$ 

VOLUME ENCLOSED TO 
$$L$$
.

 $V = \pi \int_{0}^{L} y^{2} dy = \pi \int_{0}^{L} [R^{2} - (K_{1}X)^{2}] dy$ 

$$= \pi \left[ R^{2}L - \frac{1}{2}K_{1}^{2}L_{2}^{2} \right]$$

$$= \pi L\left(\frac{R}{a}\right)^{2}(a^{2} - \frac{1}{3}L^{2})$$
 $K_{1} = R_{0}^{2}$ 

VOLUME ENCLOSED TO a (ENTIRE BULL'D)

$$V = \pi \left[ \frac{R^2 L - \frac{1}{3} K_1^2 n^3}{\text{ABOVE}} \right]$$

$$\text{WHEN } L = \alpha \text{ AND } K_1 = \frac{8}{3} \alpha$$

$$V = \pi \left[ \frac{R^2 \alpha - \frac{1}{3} \frac{R^2}{\alpha^2} \cdot \alpha^2}{\alpha^2} \right]$$

= 2/3 17 R2 a

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## ELLIPTICAL BULKHEAD (CONTD)

SURFACE AREA (BULK'D IN CYLINDRICAL TANK)

$$y^{2} = R^{2} - (K_{1}X)^{2}$$

$$K_{1} = R^{2}$$

$$K_{2} = R^{2}$$

$$K_{3} = R^{2}$$

$$K_{4} = R^{2}$$

$$K_{5} = R^{2}$$

$$= 2\pi \int_{0}^{\infty} y \, ds \qquad ds = \sqrt{1}$$

$$= 2\pi \int_{0}^{\infty} y \, \sqrt{1 + \frac{K^{4} X^{2}}{y^{2}}} \, dx$$

$$= 2\pi \int_{0}^{2} \sqrt{R^{2} - K_{1}^{2} X^{2} + K_{1}^{4} X^{2}} dX$$

= 
$$2\pi\int_0^a \sqrt{C_1x^2 + R^2} dx$$

= 
$$2\pi \left[\frac{X}{2}\sqrt{C_{1}X^{2}+R^{2}}+\frac{R^{2}}{2\sqrt{C_{1}}}Log_{1}(X\sqrt{C_{1}}+\sqrt{C_{1}X^{2}+R^{2}})\right]_{0}^{2}$$

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ELLIPTICAL BULKHEAD (CONT'D)

RADIUS OF CURVATURE (P)

$$y^{2} = R^{2} - (K_{1}X)^{2}$$

$$K_{1} = \frac{R}{\alpha}$$

$$P = \frac{\left[1 + \left(\frac{dy}{dx}\right)^{2}\right]^{\frac{3}{2}}}{\frac{d^{2}y}{dx}}$$

$$y = (R^{2} - K_{1}^{2} X^{2})^{\frac{1}{2}}$$

$$\frac{dy}{dx} = -K_{1}^{2} X (R^{2} - K_{1}^{2} X^{2})^{-\frac{1}{2}}$$

$$\frac{d\hat{y}}{d\hat{x}} = \frac{(R^2 - K_1^2 X^2)^{\frac{1}{2}} (-K_1^2 X^2)^{-\frac{1}{2}} (-K_$$

$$= \frac{(R^2 - K_1^2 X^2)^{-\frac{1}{2}} \left[ (R^2 - K_1^2 X^2 X - K_1^2) - (-K_1^2 X) + (-2K_1^2 X) \right]}{R^2 - K_1^2 X^2}$$

$$\frac{-K_{1}^{2}(R^{2}-K_{1}^{2}X^{2})-K_{1}^{4}X^{2}}{(R^{2}-K_{1}^{2}X^{2})^{2}}=\frac{-K_{1}^{2}R^{2}}{(R^{2}-K_{1}^{2}X^{2})^{2}}$$

$$= \frac{(R^2 - K_1^2 \chi^2)^{\frac{9}{2}} \left[1 + K_1^4 \chi^2 (R^2 - K_1^2 \chi^2)^{-1}\right]^{\frac{9}{2}}}{-K_1^2 R^2}$$

$$= \frac{\left[R^2 + K_1^2 \chi^2 (K_1^2 - 1)\right]^{\frac{1}{2}}}{K_1^2 R^2}$$

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(OR)

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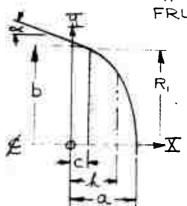
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K2 = 1/2

K2 = 1/a

ELLIPTICAL BULKHEAD (CONTD)

VOLUME (ENCLOSED BY THE BULKHEAD AT THE END OF A CONICAL FRUSTUM TANK)



GEN ELLIPTICAL EQUATION 
$$\frac{X^2}{a^2} + \frac{y^2}{b^2} = 1$$

$$y^2 = b^2 - (K_2 \times)^2$$
 $K_2 = \frac{b}{a}$ 

WHERE

D = MAJOR SEMI. AXIS a = MINOR SEMI AXIS

A PROPELLANT LEVEL

C.R. TANK (INTERSECTION OF TANK WITH BULK'D)

VOLUME ENCLOSED FROM "C" TO "L"
$$V = \pi \int_{c}^{L} y^{2} dx = \pi \int_{c}^{L} [b^{2} - (K_{2}X)^{2}] dx$$

= 
$$\pi \left[ b^2 \lambda - \frac{1}{3} K_2^2 \lambda^3 - b^2 c + \frac{1}{3} K_2^2 c^3 \right]$$

= 
$$\pi \left[ b^2 (\lambda - c) + \frac{1}{3} K_2^2 (c^3 - k^3) \right]$$

$$= \pi \left(\frac{b}{a}\right)^2 \left[\alpha^2 (\lambda - c) + \frac{1}{3} (c^3 - k^2)\right]$$

VOLUME ENCLOSED FROM "C" TO "a"
$$V = \pi \left[ b^{2}(a-c) + \frac{1}{3} K_{2}^{2}(c^{2}-a^{2}) \right]$$
(OR)
$$= \pi \left[ \frac{b}{a^{2}} \right] a^{2}(a-c) + \frac{1}{3} (c^{3}-a^{2})$$

$$= \pi \left(\frac{b}{a}\right)^2 \left[\alpha^2(\alpha-c) + \frac{1}{3}(c^3-\alpha^3)\right]$$

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SAN DIEGO, CALIFORNIA Model

Report No. ZP-7-022TN

## ELLIPTICAL BULKHEAD (CONT'D)

(BULK'D AT END OF CONICAL FRUSTUM TANK CONT'D)

GENERALLY SPEAKING THE VALUE K, (RATIO OF MAJOR TO MINOR AXIS) IS PRE-DETERMINED BY STRUCTURAL CONSIDERATIONS. ALSO THE VALUE OF R, (RADIUS OF TANK END) AND & (CONICAL FRUSTUM HALF ANGLE) ARE KNOWN FROM THE TANK GEOMETRY. FROM THESE (K2, R, \$ &) THE BULKHEAD GEOMETRY MAY BE SET AS FOLLOWS.

BULKHEAD'S MAJOR AXIS "b"

$$y^2 = b^2 - (K_2 X)^2$$
 (Basic EQUATION)  
 $b = \sqrt{y^2 + (K_2 X)^2}$ 

$$\alpha = \frac{1}{2}K$$

IF THE BULK'DS HEIGHT "H" BEYOND THE TANK END IS KNOWN IN ADDITION TO K2 R, & K THEN,

b = K2a

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SAN DIEGO, CALIFORNIA

Report No. ZP-7-022TN

### ELLIPTICAL BULKHEAD (CONT'D)

(BULK'D AT END OF CONICAL FRUSTUM TANK-CONTO)

# VALUE OF "C" AND "R

R.

C = DISTANCE BETWEEN MAJOR AXIS AND BULKHEAD INTERSECTION WITH TANK

R, TANK AND BULKHEAD INTERSECTION RADIUS (RADIUS AT TOP OF TANK) Q = BULK'D MINOR SEMI AXIS MAJOR

$$y^2 = b^2 - (K_2 x)^2$$
 BULK'D GENERAL FORMULA
$$K_2 = \frac{b}{a}$$

THE SLOPE AT ANY POINT ON ELL PSE 24 dy = 0 - 2 K2 x dx (DIFF. OF ABOVE FORMULA)

$$\frac{dy}{dy} = -\frac{2K_{2}^{2}X}{2y} = -K_{2}^{2}\frac{X}{y}$$

ALLO # = - TAN X

THEN - TAN 
$$x = -K_2 \frac{x}{y}$$
  
WHEN  $x = C$   $y = R_1$ 

TANK = K2 CR.

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### ELLIPTICAL BULKHEAD (CONTD)

(BULK'D AT END OF CONICAL FRUSTUM TANK-CONT'D) VALUE OF "C" AND "R" (CONT'D)

TAN 
$$K = K_2^2 \frac{X}{Y}$$
 (FROM PREVIOUS PAGE)  
WHEN  $X = C$   $y^2 = b^2 - (K_2 C)^2$   
 $TAN^2 K = K_2^4 \frac{X^2}{Y^2}$ 

TAN2x (b2-K2C2)= K2 C2 (K2 + K2 TAN2X)C2 = b2 TAN2X

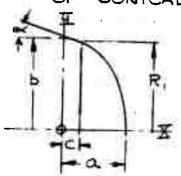
$$C = \frac{b \operatorname{TAN} \propto}{K_2 \sqrt{K_2^2 + \operatorname{TAN}^2} \propto} = \frac{b \operatorname{TAN} \propto}{\frac{b}{\alpha} \sqrt{\frac{b^2}{\alpha^2} + \operatorname{TAN}^2} \times}$$
$$= \frac{\alpha^2 \operatorname{TAN} \propto}{\sqrt{b^2 + \alpha^2 \operatorname{TAN}^2} \propto}$$

WHEN X = C y = R, THEN FROM Y2 = b2 - K2 X2 R2 = b2 - K2 C2  $R_1 = \sqrt{b^2 - \frac{b^2}{a^2}} C^2$  $= \frac{b}{a} \sqrt{\alpha^2 - C^2}$  Prepared By Checked By Revised Dete

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## ELLIPTICAL BULKHEAD (CONT'O)

SURFACE AREA (BULK'D AT SMALL EN OF CONICAL FRUSTUM TANK)



$$y^2 = b^2 - (K_2 x)^2$$
 $K_2 = \frac{b}{a}$ 

SURFACE AREA OF THE ELLIPTICAL BULK'D FROM LINE OF TANK INTERSECTION

FROM WHICH, (SEE DEVEL. ON PREVIOUS PAGE) 5 = 211 ( 1/C2 x2 + b2 dx

WHERE C2 = K2 - K2

WHERE: Q = BULK'D MINOR SEMI AXIS (HEIGHT) MAJOR C = DIST. BETWEEN MAJOR AXIS AND BULK'S

INTERSECT WITH TANK - B. TANK C, = K1 - K2 WHERE K2 = 1/0 LOG IS TO BASE "E"

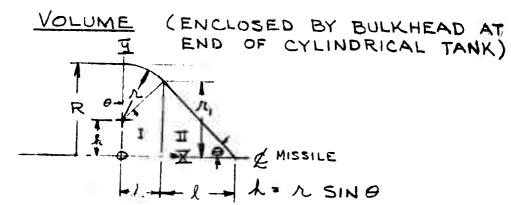
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### TORICONICAL BULKHEAD



### VOLUME I

$$X^{2} + (y - h)^{2} = h^{2}$$

$$y^{2} = h^{2} + 2h\sqrt{h^{2} - y^{2}} + h^{2} - x^{2}$$

$$y^{3} = h^{2} + 2h\sqrt{h^{2} - y^{2}} + h^{2} - x^{2}$$

$$V_{1} = \pi \int_{0}^{h} y^{2} dx = \pi \int_{0}^{h} (h^{2} + 2h\sqrt{h^{2} - x^{2}} + h^{2} - x^{2}) dx$$

$$= \pi \left\{ h^{2}x + 2h \cancel{x} [x\sqrt{h^{2} - x^{2}} + h^{2} sin(\cancel{x})] + h^{2}x - \cancel{x}^{3} \right\}_{0}^{h}$$

$$= \pi \left\{ h(h^{2} + h^{2}) + h [h\sqrt{h^{2} - L^{2}} + h^{2} sin(\cancel{x})] - \cancel{x}^{3} \right\}_{0}^{h}$$

### VOLUME I

$$V = \frac{1}{3} \text{ AB } 2$$
 (GENERAL CONE FORMULA)  
=  $\frac{1}{3} \text{ Th} \chi_1^2 \times \Lambda_1 \text{Cot } \Theta$   
=  $\frac{1}{3} \text{ Th} \chi_1^3 \text{ Cot } \Theta$ 

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### TORICONICAL BULK'D (CONT'D)

SURFACE ENCLOSING VOLUME I

$$S_1 = 2\pi \int_0^L \left(h + \sqrt{\Lambda^2 - X^2}\right) \left[1 + \frac{X^2}{\Lambda^2 - X^2}\right]^{\frac{1}{2}} d\gamma$$

= 
$$2\pi \Lambda \left[ k \sin^{-1}\left(\frac{X}{A}\right) + X \right]^{L}$$

= 2 11 / [ h SIN (X) + h]

SURFACE ENCLOSING VOLUME II

SI = AREA OF BASE = 11 12 (CLASSIC)

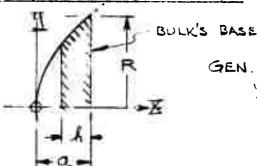
TOTAL SURF. AREA OF TORICONICAL BULKO IS:

- 1777 C

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### PARABOLIC BULKHEAD



GEN. PARABOLIC EQUATION

$$A = \frac{R^2}{a}$$

VOLUME ENCLOSED FROM " TO " (SHADED) V=T) y2dx = T( Axdx

= 
$$\pi \frac{R^2}{a} \int_{a-L}^{L} x dx$$

= 
$$\frac{11 \text{ a}}{2a} \int_{a-k}^{x} dx$$
  
=  $\frac{11 \text{ R}^2}{2a} \times \left[a^2 - (a-k)^2\right]$ 

WHEN L = a THEN,

SURFACE AREA OF ENTIRE BULKD

= 
$$\Pi \left[ \frac{2}{3/4A} \left( 4Ax + A^2 \right)^{\frac{1}{2}} \right]_0^2 = \frac{\Pi}{6A} \left[ \left( 4Aa + A^2 \right)^{\frac{1}{2}} - A^3 \right]$$

$$= \frac{\pi R^{3}}{GA} \left[ \left( 4 + \frac{R^{3}}{a^{3}} \right)^{2} - \frac{R^{3}}{a^{3}} \right] = \frac{\pi Ra}{G} \left[ \left( 4 + \frac{R^{3}}{a^{3}} \right)^{2} - \left( \frac{R}{G} \right)^{3} \right]$$

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PARABOLIC BULK'D CONT'D

RADIUS OF CURVATURE (P) A = R/a

$$y = A^{\frac{1}{2}} X^{\frac{1}{2}}$$
  $\frac{dy}{dx} = \frac{1}{2} A^{\frac{1}{2}} X^{\frac{1}{2}}$   $\frac{dx}{dx} = -\frac{1}{4} A^{\frac{1}{2}} X^{-\frac{3}{2}}$ 

$$\frac{\left[1 + \left(\frac{1}{2} A^{\frac{1}{2}} X^{-\frac{1}{2}}\right)^{2}\right]^{\frac{1}{2}}}{-\frac{1}{4} A^{\frac{1}{2}} X^{-\frac{3}{2}}}$$

$$\frac{\left[1 + \frac{1}{4} A X^{-1}\right]^{\frac{3}{2}}}{-\frac{1}{4} A^{\frac{1}{2}} Y^{-\frac{3}{2}}}$$

$$\frac{\left[1 + \frac{1}{4} A X^{-1}\right]^{\frac{3}{2}}}{-\frac{1}{4} A^{\frac{1}{2}} X^{-\frac{3}{2}}} - 4 X^{\frac{1}{2}} \left(\frac{4X + A}{4X}\right)^{\frac{3}{2}} = \frac{-4 X^{\frac{1}{2}} (4X + A)^{\frac{3}{2}}}{8 X^{\frac{1}{2}} A^{\frac{1}{2}}}$$

$$A \cdot \vec{a}^{2} = \frac{1}{2} \frac{(4x + R^{2})^{3/2}}{(R^{2})^{2}}$$

$$= \frac{1}{2Ra} (4ax + R^{2})^{3/2}$$

\* NOTE: THE MINUS SIGN APPEARING NO SIGNIFIGANCE AND IS THEFORE DROPPED FROM THE EQUATION .

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TORUS

$$x^{2} + (y - b)^{2} \cdot a^{2}$$
  
 $y - b = \pm \sqrt{a^{2} - x^{2}}$   
 $y = b \pm \sqrt{a^{2} - x^{2}}$ 

SURFACE AREA

dy = + x(a2-x2)2

AREA GENERATED BY REVOLVING THE UPPER S  

$$S_u = 271 \int_{-a}^{a} (b + \sqrt{a^2 - x^2}) \left[ 1 + \frac{x^2}{a^2 - x^2} \right]_{a}^{1/2} dx$$

AREA GENERATED BY REVOLVING THE LOWER SEMI-CIRCLE  $S_{L} = 2\pi \int_{-\infty}^{\infty} (b - \sqrt{a^{2} + x^{2}}) \left[1 + \frac{x^{2}}{a^{2} - x^{2}}\right]^{1/2} dx$ 

TOTAL SURFACE AREA ST = Sut SL

= 
$$2\pi \int_{a}^{a} 2b ds$$
  
=  $4\pi b \int_{a}^{a} \left[1 + \frac{x^{2}}{a^{2} - x^{2}}\right]^{1/2} dx = 4\pi b \int_{a}^{a} \left(\frac{a^{2}}{a^{2} - x^{2}}\right)^{1/2} dx$ 

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TORUS (CONT'D)

$$5_{1}$$
 = 4  $\pi$  a b  $\left(\sin^{-1}\frac{x}{a}\right)$  + c  $\left[\cos^{-1}\frac{x}{a}\right]$ 

= 4 
$$\pi$$
 a b  $\left[\sin^{-1}(1) - \sin^{-1}(-1)\right]$   
= 4  $\pi$  a b  $\left[2 \frac{\pi}{2}\right]$ 

VOLUME (ENCLOSED BY TORUS)

$$V_T = \pi \int_a^a (y^2 - y^2) dx$$

= 
$$\pi \int_{a}^{a} [(b + \sqrt{a^2 - X^2})^2 - (b - \sqrt{a^2 - X^2})] dx$$

= 
$$\pi \int_{a}^{a} [b^{2} + 2bV + a^{2} - x^{2} - b^{2} + 2bV - a^{2} + x^{2}] dx$$
  
=  $4\pi b \int_{a}^{a} \sqrt{a^{2} - x^{2}} dx$ 

= 
$$2 \pi b \left[ a^{2}, \frac{\pi}{2} - a^{2}, \left(-\frac{\pi}{2}\right) \right]$$

$$= 2 \pi b \left[ 2a^2 \times \frac{\pi}{2} \right]$$

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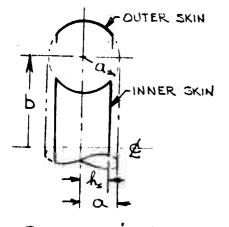
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## TORUS (CONT'D)

THE DESIGN OF A TORUS TANK IS USUALLY SUCH THAT HIGH STRESSES ARE DEVELOPED IN THE SKIN OF THE "DO.NUT" HOLE WHILE THE TANK IS UNDER PRESSURE. THIS OFTEN DICTATES HEAVIER GAGE SKINS IN THIS AREA. ALSO LIGHTER SKINS ON THE OUTSIDE OF THE TORUS. THE FOLLOWING FORMULAS ARE DEVELOPED FOR THESE LOCAL AREAS.



$$X^{2} + (y - b)^{2} = \alpha^{2}$$
  
 $\begin{cases} y_{0} = b + \sqrt{\alpha^{2} - X^{2}} & (UPPER) \\ y_{1} = b - \sqrt{\alpha^{2} - X^{2}} & (LOWER) \end{cases}$ 

SURFACE AREA OF OUTER SKIN (2 L. WIDE)

= 47 a ( b 51N (2) + h.s) \*

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### TORUS (CONT'D)

$$S_{1} = 2 \times 2\pi \int_{0}^{L} y_{1} ds$$

$$= 4\pi \int_{0}^{L} (b - \sqrt{a^{2} - x^{2}}) \left[1 + \frac{x^{2}}{a^{2} \cdot x^{2}}\right]^{L} dx$$

$$= 4\pi a \left[\frac{b}{\sqrt{a^{2} \cdot x^{2}}} - 1\right] dx$$

$$= 4\pi a \left[\frac{b}{\sqrt{a^{2} \cdot x^{2}}} - x\right]_{0}^{L}$$

$$= 4\pi a \left[\frac{b}{\sqrt{a^{2} \cdot x^{2}}} - x\right]_{0}^{L}$$

$$= 4\pi a \left[\frac{b}{\sqrt{a^{2} \cdot x^{2}}} - x\right]_{0}^{L}$$

### CHECK FOR ABOVE S' & S' EQUATIONS :

FOR TOTAL AREA OF TORUS)

\* NOTE: SIN-(a) IS DEFINED AS THE ANGLE WHOSE SINE IS TO EVALUATE THIS FUNCTION FIND TO VALUE IN A TRIG. SINE TABLE TO OBTAIN IT'S CORRESPONDING ANGLE IN DEGREES. MULTIPLY THE DEGREES BY .01745 TO OBTAIN RADIANS WHICH IS PLUGGED DIRECTLY INTO THE FORMULA IN PLACE OF "SIN-(a)".

TORUS (CONT'D)

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VOLUME OF PARTIALLY FILLED TORUS TAN

$$X^{2}+(y-b)^{2}=a^{2}$$

VOLUME OF FULL TANK
$$= 2 \pi^{2} b a^{2}$$
 (SEE PG. 23)

THIS IN THE FORMULA ABOVE, THEN